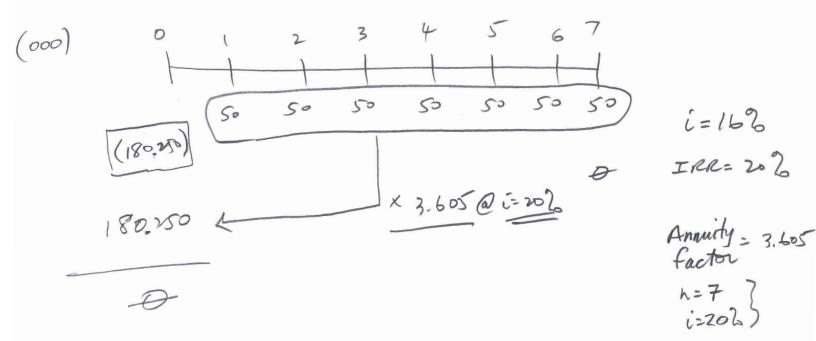
## **CAPITAL BUDGETING PRACTICE QUIZ**

28. (Ignore income taxes in this problem.) The Baker Company purchased a piece of equipment with the following expected results:

Useful life	7 years
Yearly net cash inflow	\$50,000
Salvage value	\$0
Internal rate of return	20%
Discount rate	16%

The initial cost of the equipment was:

- A. \$300,100
- B. \$180,250
- C. \$190,600
- D. Cannot be determined from the given information.



# **CAPITAL BUDGETING PRACTICE QUIZ**

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The initial cost of the equipment was:

A. \$300,100

B. \$180,250

C. \$190,600

D. Cannot be determined from the given information.

The internal rate of return is the rate of return at which the net present value of the project is zero.

				Present
		Amount of	20%	Value of
Item	Year(s)	Cash Flow	Factor	Cash Flows
Initial investment	Now	(X)	1.000	(X)
Yearly net cash inflow	1-7	\$50,000	3.605	\$180,250
Net present value				\$0

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-01 Evaluate the acceptability of an investment project using the net

present value method

Learning Objective: 13-02 Evaluate the acceptability of an investment project using the internal

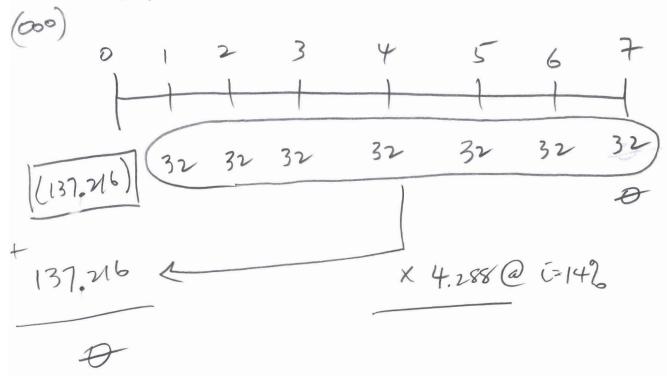
rate of return method

29. (Ignore income taxes in this problem.) The Yates Company purchased a piece of equipment which is expected to have a useful life of 7 years with no salvage value at the end of the 7-year period. This equipment is expected to generate a cash inflow of \$32,000 each year of its useful life. If this investment has a internal rate of return of 14%, then the initial cost of the equipment is:

A. \$150,000 B. \$137,216

C. \$12,800

D. \$343,360



29. (Ignore income taxes in this problem.) The Yates Company purchased a piece of equipment which is expected to have a useful life of 7 years with no salvage value at the end of the 7-year period. This equipment is expected to generate a cash inflow of \$32,000 each year of its useful life. If this investment has a internal rate of return of 14%, then the initial cost of the equipment is:

A. \$150,000

B. \$137,216

C. \$12,800

D. \$343,360

The internal rate of return is the rate of return at which the net present value of the project is zero.

				Present
		Amount of	14%	Value of
Item	Year(s)	Cash Flow	Factor	Cash Flows
Initial investment	Now	(X)	1.000	(X)
Yearly net cash inflow	1-7	\$32,000	4.288	\$137,216
Net present value				\$0

-X + \$137,216 = \$0 X = \$137,216

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-01 Evaluate the acceptability of an investment project using the net

present value method

Learning Objective: 13-02 Evaluate the acceptability of an investment project using the internal

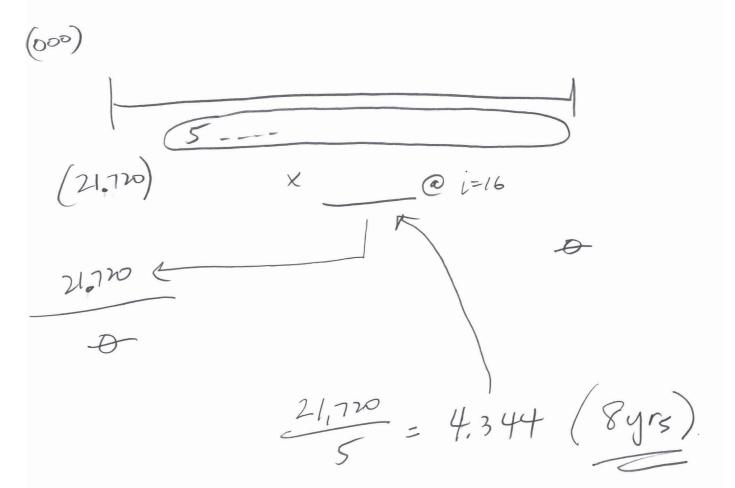
rate of return method

# 30. (Ignore income taxes in this problem.) The following information is available on a new piece of equipment:

Cost of the equipment	\$21,720
Salvage value	\$0
Annual cash inflows	\$5,000
Internal rate of return	16%
Required rate of return	10%

The life of the equipment is approximately:

- A. 6 years
- B. 4.3 years
- C. 8 years
- D. It is impossible to determine from the data given.



30. (Ignore income taxes in this problem.) The following information is available on a new piece of equipment:

Cost of the equipment	\$21,720
Salvage value	\$0
Annual cash inflows	\$5,000
Internal rate of return	16%
Required rate of return	10%

The life of the equipment is approximately:

- A. 6 years
- B. 4.3 years
- C. 8 years
- D. It is impossible to determine from the data given.

Factor of the internal rate of return = Investment required ÷ Annual net cash inflow

- $= $21,720 \div $5,000$
- = 4.344

The factor of 4.344 for 8 years represents an internal rate of return of 16%.

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-01 Evaluate the acceptability of an investment project using the net

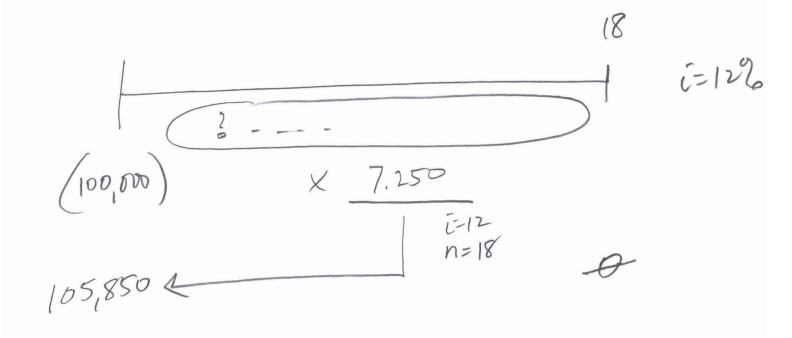
present value method

Learning Objective: 13-02 Evaluate the acceptability of an investment project using the internal

rate of return method

34. (Ignore income taxes in this problem.) Benz Company is considering the purchase of a machine that costs \$100,000, has a useful life of 18 years, and no salvage value. The company's discount rate is 12%. If the machine's net present value is \$5,850, then the annual cash inflows associated with the machine must be (round to the nearest whole dollar):

- A. \$42,413
- B. \$14,600
- C. \$13,760
- D. It is impossible to determine from the data given.



5,850 = NPV

34. (Ignore income taxes in this problem.) Benz Company is considering the purchase of a machine that costs \$100,000, has a useful life of 18 years, and no salvage value. The company's discount rate is 12%. If the machine's net present value is \$5,850, then the annual cash inflows associated with the machine must be (round to the nearest whole dollar):

A. \$42,413

B. \$14,600

C. \$13,760

D. It is impossible to determine from the data given.

Item	Year(s)	Amount of	12%	Present Value
		Cash Flow	<b>Factor</b>	of Cash Flows
Initial investment	Now	\$(100,000)	1.000	\$(100,000)
Annual cash inflows	1-18	X	7.250	7.250X
Net present value				\$5,850

-\$100,000 + 7.250X = \$5,850 7.250X = \$100,000 + \$5,850 X = (\$100,000 + \$5,850) ÷ 7.250 = \$14,600

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-01 Evaluate the acceptability of an investment project using the net

present value method

(70,000 - 05V) = (0,000/yr SL 7yrs (noncash).

62. (Ignore income taxes in this problem.) The Jackson Company has invested in a machine that cost \$70,000, that has a useful life of seven years, and that has no salvage value at the end of its useful life. The machine is being depreciated by the straight-line method, based on its useful life. It will have a payback period of four years. Given these data, the simple rate of return on the machine is closest to:

A. 7.1%

B. 8.2%

C. 10.7%

D. 39.3%

Annual Incremental NI (17,500-19,000)

Initial Investment 79,000 = 10

Paybach =

Investment Required 70,000

Annual Net Cash Inflow

17,500

62. (Ignore income taxes in this problem.) The Jackson Company has invested in a machine that cost \$70,000, that has a useful life of seven years, and that has no salvage value at the end of its useful life. The machine is being depreciated by the straight-line method, based on its useful life. It will have a payback period of four years. Given these data, the simple rate of return on the machine is closest to:

A. 7.1% B. 8.2%

<u>C.</u> 10.7%

D. 39.3%

\*Payback period = Investment required ÷ Annual net cash inflow 4 years = \$70,000 ÷ Annual net cash inflow Annual net cash inflow = \$70,000 ÷ 4 years = \$17,500 yearly cash flow

Simple rate of return = Annual incremental net operating income  $\div$  Initial investment =  $\$7,500 \div \$70,000 = 10.70\%$ 

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-05 Determine the payback period for an investment Learning Objective: 13-06 Compute the simple rate of return for an investment

(189,00-05V) = (8,000/yr.

(0 ys. Sc Degroe
(non-cash).

69. (Ignore income taxes in this problem.) Blaine Corporation is considering replacing a technologically obsolete machine with a new state-of-the-art numerically controlled machine. The new machine would cost \$180,000 and would have a ten-year useful life. Unfortunately, the new machine would have no salvage value. The new machine would cost \$12,000 per year to operate and maintain, but would save \$48,000 per year in labor and other costs. The old machine can be sold now for scrap for \$20,000. What is the simple rate of return on the new machine (round off your answer to the nearest one-hundredth of a percent)?

A. 10.00%

B. 26.67%

C. 22.50%

D. 11.25%

Annual Incremental
NI

Initial Investment

48,000 - 12,000 - 18,000

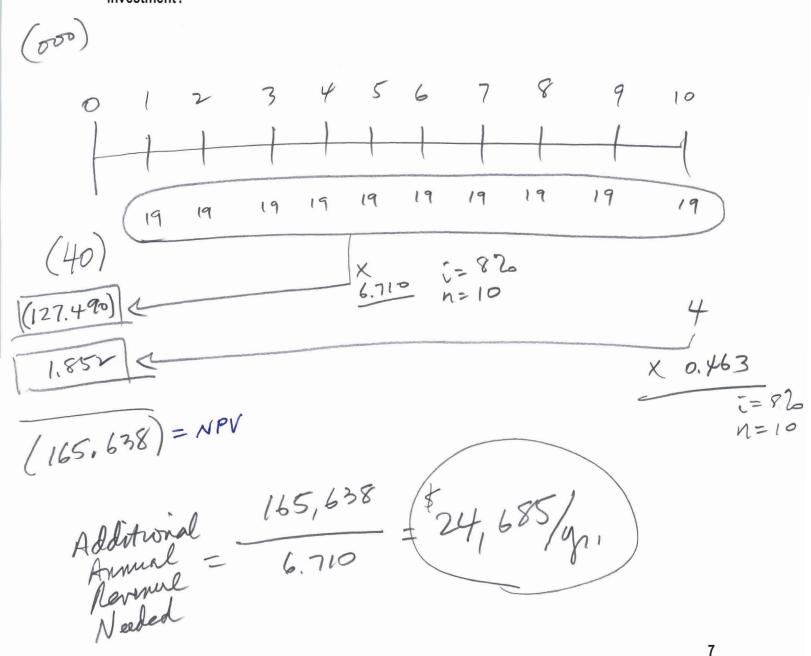
180,000 - 20,000

= 11.75%

136. (Ignore income taxes in this problem.) The management of an amusement park is considering purchasing a new ride for \$40,000 that would have a useful life of 10 years and a salvage value of \$4,000. The ride would require annual operating costs of \$19,000 throughout its useful life. The company's discount rate is 8%. Management is unsure about how much additional ticket revenue the new ride would generate-particularly because customers pay a flat fee when they enter the park that entitles them to unlimited rides. Hopefully, the presence of the ride would attract new customers.

### Required:

How much additional revenue would the ride have to generate per year to make it an attractive investment?



136. (Ignore income taxes in this problem.) The management of an amusement park is considering purchasing a new ride for \$40,000 that would have a useful life of 10 years and a salvage value of \$4,000. The ride would require annual operating costs of \$19,000 throughout its useful life. The company's discount rate is 8%. Management is unsure about how much additional ticket revenue the new ride would generate-particularly because customers pay a flat fee when they enter the park that entitles them to unlimited rides. Hopefully, the presence of the ride would attract new customers.

#### Required:

How much additional revenue would the ride have to generate per year to make it an attractive investment?

Item	Year(s)	Amount of Cash Flow	8% Factor	Present Value of Cash Flows
Initial investment	Now	\$(40,000)	1.000	\$ (40,000)
Annual operating costs	1-10	\$(19,000)	6.710	(127,490)
Salvage value	10	\$4,000	0.463	1,852
Net present value				\$(165,638)

Minimum annual cash flows required = Negative net present value to be offset ÷ Present value factor

 $$165,638 \div 6.710 = $24,685$ 

This much additional revenue would result in a zero net present value. Any less than this and the net present value would be negative. Any more than this and the net present value would be positive.

AACSB: Analytic

AICPA BB: Critical Thinking AICPA FN: Measurement Bloom's: Application

Learning Objective: 13-03 Evaluate an investment project that has uncertain cash flows

LUMP SUM

3.4.         4.6. <th< th=""><th>+ 1)</th><th><math>+ \eta^n</math>. In this table <math>S = \$1.00</math>.</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>-</th><th></th><th></th><th></th><th></th><th>١</th><th></th><th></th><th></th><th></th></th<>	+ 1)	$+ \eta^n$ . In this table $S = $1.00$ .								-					١				
0.986         0.967         0.867         0.867         0.867         0.869         0.899 <th< th=""><th>Periods</th><th>2%</th><th>4%</th><th>969</th><th>8%</th><th>10%</th><th>12%</th><th>14%</th><th>16%</th><th>18%</th><th>20%</th><th>22%</th><th>24%</th><th>76%</th><th>28%</th><th>30%</th><th>32%</th><th>40%</th><th>Periods</th></th<>	Periods	2%	4%	969	8%	10%	12%	14%	16%	18%	20%	22%	24%	76%	28%	30%	32%	40%	Periods
0.954         0.859         0.859         0.857         0.856         0.753         0.754 <th< td=""><td>1</td><td>0.980</td><td>0.962</td><td>0.943</td><td>0.926</td><td>0.909</td><td>0.893</td><td>0.877</td><td>0.862</td><td>0.847</td><td>0.833</td><td>0.820</td><td>908.0</td><td>0.794</td><td>0.781</td><td>0.769</td><td>0.758</td><td>0.714</td><td>1</td></th<>	1	0.980	0.962	0.943	0.926	0.909	0.893	0.877	0.862	0.847	0.833	0.820	908.0	0.794	0.781	0.769	0.758	0.714	1
0.942         0.889         0.844         0.734         0.254         0.635         0.673 <th< td=""><td>2</td><td>0.961</td><td>0.925</td><td>0.890</td><td>0.857</td><td>0.826</td><td>0.797</td><td>0.769</td><td>0.743</td><td>0.718</td><td>0.694</td><td>0.672</td><td>0.650</td><td>0.630</td><td>0.610</td><td>0.592</td><td>0.574</td><td>0.510</td><td>7</td></th<>	2	0.961	0.925	0.890	0.857	0.826	0.797	0.769	0.743	0.718	0.694	0.672	0.650	0.630	0.610	0.592	0.574	0.510	7
9.994         0.885         0.735         0.654         0.659         0.659         0.659         0.659         0.659         0.759         0.734         0.885         0.799         0.734         0.885         0.799         0.734         0.885         0.799         0.734         0.885         0.799         0.759         0.759         0.659         0.654         0.657         0.549         0.476         0.437         0.379         0.349         0.279         0.219         0.175         0.259         0.259         0.259         0.259         0.659 <th< td=""><td>m</td><td>0.942</td><td>0.889</td><td>0.840</td><td>0.794</td><td>0.751</td><td>0.712</td><td>0.675</td><td>0.641</td><td>609.0</td><td>0.579</td><td>0.551</td><td>0.524</td><td>0.500</td><td>0.477</td><td>0.455</td><td>0.435</td><td>0.364</td><td>3</td></th<>	m	0.942	0.889	0.840	0.794	0.751	0.712	0.675	0.641	609.0	0.579	0.551	0.524	0.500	0.477	0.455	0.435	0.364	3
0.883         0.824         0.874         0.681         0.875 <th< td=""><td>4</td><td>0.924</td><td>0.855</td><td>0.792</td><td>0.735</td><td>0.683</td><td>0.636</td><td>0.592</td><td>0.552</td><td>0.516</td><td>0.482</td><td>0.451</td><td>.0.423</td><td>0.397</td><td>0.373</td><td>0.350</td><td>0.329</td><td>0.260</td><td>4</td></th<>	4	0.924	0.855	0.792	0.735	0.683	0.636	0.592	0.552	0.516	0.482	0.451	.0.423	0.397	0.373	0.350	0.329	0.260	4
0.881         0.790         0.875         0.689         0.579         0.488         0.790         0.876         0.687         0.488         0.790         0.879         0.687         0.687         0.486         0.489         0.237         0.249         0.234         0.234         0.234         0.234         0.234         0.234         0.224         0.189         0.273         0.024         0.035         0.034         0.035         0.034         0.035         0.034         0.034         0.034         0.035         0.034         0.035         0.034         0.035         0.034         0.034         0.035         0.034         0.034         0.035         0.034         0.034         0.035         0.034 <th< td=""><td>m</td><td>906.0</td><td>0.822</td><td>0.747</td><td>0.681</td><td>0.621</td><td>0.567</td><td>0.519</td><td>0.476</td><td>0.437</td><td>0.402</td><td>0.370</td><td>0.341</td><td>0.315</td><td>0.291</td><td>0.269</td><td>0.250</td><td>0.186</td><td>2</td></th<>	m	906.0	0.822	0.747	0.681	0.621	0.567	0.519	0.476	0.437	0.402	0.370	0.341	0.315	0.291	0.269	0.250	0.186	2
0.837         0.746         0.746         0.746         0.746         0.746         0.746         0.746         0.746         0.749         0.749         0.749         0.749         0.749         0.749         0.749         0.749         0.749         0.749         0.744         0.749         0.744         0.749         0.744 <th< td=""><td>9</td><td>0.888</td><td>0.790</td><td>0.705</td><td>0.630</td><td>0.564</td><td>0.507</td><td>0.456</td><td>0.410</td><td>0.370</td><td>0.335</td><td>0.303</td><td>0.275</td><td>0.250</td><td>0.227</td><td>0.207</td><td>0.189</td><td>0.133</td><td>9</td></th<>	9	0.888	0.790	0.705	0.630	0.564	0.507	0.456	0.410	0.370	0.335	0.303	0.275	0.250	0.227	0.207	0.189	0.133	9
0.837         0.731         0.647         0.449         0.451         0.469         0.451         0.469         0.451         0.469         0.451         0.469         0.449         0.431         0.269         0.144         0.143         0.115         0.115         0.115         0.115         0.114         0.115         0.115         0.116         0.029         0.0242         0.0242         0.2242         0.2429         0.1249         0.1249         0.1249         0.0449         0.049	7	0.871	0.760	0.665	0.583	0.513	0.452	0.400	0.354	0.314	0.279	0.249	0.222	0.198	- 0.178	0.159	0.143	0.095	7
0.837         0.703         0.552         0.504         0.434         0.263         0.223         0.124         0.157         0.114         0.115         0.103         0.003 <th< td=""><td>80</td><td>0.853</td><td>0.731</td><td>0.627</td><td>0.540</td><td>0.467</td><td>0.404</td><td>0.351</td><td>0.305</td><td>0.266</td><td>0.233</td><td>0.204</td><td>0.179</td><td>0.157</td><td>0.139</td><td>0.123</td><td>0.108</td><td>890.0</td><td>8</td></th<>	80	0.853	0.731	0.627	0.540	0.467	0.404	0.351	0.305	0.266	0.233	0.204	0.179	0.157	0.139	0.123	0.108	890.0	8
0.820         0.657         0.558         0.443         0.236         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.239         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.237         0.137         0.137         0.137         0.137         0.137         0.043         0.056         0.056         0.056         0.056         0.056         0.056         0.057 <th< td=""><td>6</td><td>0.837</td><td>0.703</td><td>0.592</td><td>0.500</td><td>0.424</td><td>0.361</td><td>0.308</td><td>0.263</td><td>0.225</td><td>0.194</td><td>0.167</td><td>0.144</td><td>0.125</td><td>0.108</td><td>0.094</td><td>0.082</td><td>0.048</td><td>6</td></th<>	6	0.837	0.703	0.592	0.500	0.424	0.361	0.308	0.263	0.225	0.194	0.167	0.144	0.125	0.108	0.094	0.082	0.048	6
0.884         0.650         0.527         0.429         0.357         0.287         0.195         0.195         0.115         0.115         0.014         0.004         0.005         0.024         0.025         0.043         0.135         0.135         0.135         0.118         0.118         0.118         0.018         0.018         0.025         0.040         0.025         0.020         0.040         0.025 <th< td=""><td>10</td><td>0.820</td><td>9290</td><td>0.558</td><td>0.463</td><td>0.386</td><td>0.322</td><td>0.270</td><td>0.227</td><td>0.191</td><td>0.162</td><td>0.137</td><td>0.116</td><td>660.0</td><td>0.085</td><td>0.073</td><td>0.062</td><td>0.035</td><td>10</td></th<>	10	0.820	9290	0.558	0.463	0.386	0.322	0.270	0.227	0.191	0.162	0.137	0.116	660.0	0.085	0.073	0.062	0.035	10
0.738         0.625         0.497         0.397         0.239         0.218         0.112         0.092         0.076         0.052         0.043         0.037         0.018           0.738         0.6451         0.4480         0.348         0.6451         0.448         0.648         0.048         0.048         0.049         0.079	11	0.804	0.650	0.527	0.429	0.350	0.287	0.237	0.195	0.162	0.135	0.112	0.094	0.079	990.0	0.056	0.047	0.025	11
0.773         0.601         0.469         0.366         0.229         0.125         0.114         0.116         0.035         0.047         0.040         0.039         0.077         0.040         0.039         0.077         0.040         0.039         0.037         0.040         0.039         0.077         0.040         0.039         0.077         0.040         0.039         0.077         0.040         0.039         0.077         0.040         0.039         0.077         0.040         0.039         0.078         0.042         0.039         0.039         0.074         0.043         0.034         0.024         0.039         0.034         0.040         0.039         0.034         0.040         0.034         0.034         0.040         0.034         0.034         0.040         0.034         0.034         0.044         0.044         0.034         0.024         0.034         0.042         0.034 <th< td=""><td>12</td><td>0.788</td><td>0.625</td><td>0.497</td><td>0.397</td><td>0.319</td><td>0.257</td><td>0.208</td><td>0.168</td><td>0.137</td><td>0.112</td><td>0.092</td><td>920.0</td><td>0.062</td><td>0.052</td><td>0.043</td><td>0.036</td><td>0.018</td><td>12</td></th<>	12	0.788	0.625	0.497	0.397	0.319	0.257	0.208	0.168	0.137	0.112	0.092	920.0	0.062	0.052	0.043	0.036	0.018	12
0.738         0.577         0.442         0.349         0.263         0.078         0.078         0.078         0.079         0.079         0.078         0.079 <th< td=""><td>13</td><td>0.773</td><td>0.601</td><td>0.469</td><td>0.368</td><td>0.290</td><td>0,229</td><td>0.182</td><td>0.145</td><td>0.116</td><td>0.093</td><td>0.075</td><td>0.061</td><td>0.050</td><td>0.040</td><td>0.033</td><td>0.027</td><td>0.013</td><td>- 13</td></th<>	13	0.773	0.601	0.469	0.368	0.290	0,229	0.182	0.145	0.116	0.093	0.075	0.061	0.050	0.040	0.033	0.027	0.013	- 13
0.738         0.555         0.417         0.315         0.239         0.183         0.140         0.004         0.0041         0.0031         0.0045         0.0040         0.0031         0.0045         0.0045         0.0041         0.0045         0.0045         0.0041         0.0045	14	0.758	0.577	0.442	0.340	0.263	0.205	0.160	0.125	0.099	0.078	0.062	0.049	0.039	0.032	0.025	0.021	0.009	14
0.728         0.534         0.394         0.292         0.218         0.133         0.103         0.013         0.071         0.054         0.024         0.025         0.019         0.010         0.035         0.034         0.024         0.034         0.025         0.034         0.034         0.035         0.034         0.034         0.026         0.045         0.049 <th< td=""><td>15</td><td>0.743</td><td>0.555</td><td>0.417</td><td>0.315</td><td>0.239</td><td>0.183</td><td>0.140</td><td>0.108</td><td>0.084</td><td>0.065</td><td>0.051</td><td>0.040</td><td>0.031</td><td>0.025</td><td>0.020</td><td>0.016</td><td>9000</td><td>15</td></th<>	15	0.743	0.555	0.417	0.315	0.239	0.183	0.140	0.108	0.084	0.065	0.051	0.040	0.031	0.025	0.020	0.016	9000	15
0.714         0.513         0.371         0.270         0.198         0.146         0.108         0.080         0.045         0.034         0.026         0.020         0.034         0.020         0.015         0.030         0.003         0.003           0.700         0.494         0.350         0.250         0.180         0.130         0.069         0.069         0.051         0.038         0.021         0.017         0.016         0.017         0.016         0.017         0.016         0.017         0.017         0.019         0.007         0.007         0.007         0.007         0.007         0.002         0.002         0.004         0.004         0.014         0.014         0.014         0.014         0.014         0.014         0.014         0.014         0.014         0.014         0.024         0.014         0.014         0.024         0.014         0.014         0.024         0.044         0.024         0.044         0.034         0.024         0.014         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.044         0.0	18	0.728	0.534	0.394	0.292	0.218	0.163	0.123	0.093	0.071	0.054	0.042	0.032	0.025	0.019	0.015	0.012	0.005	16
0.700         0.494         0.350         0.250         0.014         0.025         0.130         0.021         0.038         0.021         0.010         0.010         0.001         0.001         0.000         0.000         0.000         0.000         0.001         0.001         0.000         0.000         0.000         0.001 <th< td=""><td>17</td><td>0.714</td><td>0.513</td><td>0.371</td><td>0.270</td><td>0.198</td><td>0.146</td><td>0.108</td><td>0.080</td><td>0.060</td><td>0.045</td><td>0.034</td><td>0.026</td><td>0.020</td><td>0.015</td><td>0.012</td><td>0.009</td><td>0.003</td><td>17</td></th<>	17	0.714	0.513	0.371	0.270	0.198	0.146	0.108	0.080	0.060	0.045	0.034	0.026	0.020	0.015	0.012	0.009	0.003	17
0.686         0.475         0.331         0.232         0.164         0.116         0.083         0.064         0.031         0.031         0.031         0.030         0.007         0.005         0.007         0.005         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.002         0.003         0.004         0.031         0.032         0.004         0.033         0.026         0.033         0.026         0.034 <th< td=""><td>18</td><td>0.700</td><td>0.494</td><td>0.350</td><td>0.250</td><td>0.180</td><td>0.130</td><td>0.095</td><td>0.069</td><td>0.051</td><td>0.038</td><td>0.028</td><td>0.021</td><td>0.016</td><td>0.012</td><td>600.0</td><td>0.007</td><td>0.002</td><td>18</td></th<>	18	0.700	0.494	0.350	0.250	0.180	0.130	0.095	0.069	0.051	0.038	0.028	0.021	0.016	0.012	600.0	0.007	0.002	18
0.6543         0.456         0.312         0.214         0.1044         0.015         0.015         0.014         0.015         0.014         0.015         0.014         0.015         0.014         <	19	0.686	0.475	0.331	0.232	0.164	0.116	0.083	0.060	0.043	0.031	0.023	0.017	0.012	0.009	0.007	0.005	0.002	19
0.660         0.439         0.294         0.135         0.035         0.044         0.031         0.025         0.011         0.008         0.006         0.004         0.009 <th< td=""><td>20</td><td>0.673</td><td>0.456</td><td>0.312</td><td>0.215</td><td>0.149</td><td>0.104</td><td>0.073</td><td>0.051</td><td>0.037</td><td>0.026</td><td>0.019</td><td>0.014</td><td>0.010</td><td>0.007</td><td>0.005</td><td>0.004</td><td>0.001</td><td>. 20</td></th<>	20	0.673	0.456	0.312	0.215	0.149	0.104	0.073	0.051	0.037	0.026	0.019	0.014	0.010	0.007	0.005	0.004	0.001	. 20
0.647         0.422         0.278         0.184         0.123         0.084         0.036         0.013         0.001         0.002         0.004         0.009         0.004         0.009         0.000         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.001         0.002         0.001         0.001         0.001         0.001         0.002         0.001         0.001         0.002         0.001         0.001         0.002         0.002         0.001         0.001         0.002         0.002         0.001         0.001         0.002         0.003         0.002         0.001         0.002         0.003         0.002         0.001         0.000         0.002         0.001         0.000         0.001         0.000         0.000         0.001         0.000         0.001         0.002 <th< td=""><td>21</td><td>0.660</td><td>0.439</td><td>0.294</td><td>0.199</td><td>0.135</td><td>0.093</td><td>0.064</td><td>0.044</td><td>0.031</td><td>0.022</td><td>0.015</td><td>0.011</td><td>0.008</td><td>0.006</td><td>0.004</td><td>0.003</td><td>0.001</td><td>21</td></th<>	21	0.660	0.439	0.294	0.199	0.135	0.093	0.064	0.044	0.031	0.022	0.015	0.011	0.008	0.006	0.004	0.003	0.001	21
0.634         0.406         0.262         0.170         0.112         0.044         0.043         0.033         0.010         0.007         0.005         0.003         0.002         0.000 <th< td=""><td>22</td><td>0.647</td><td>0.422</td><td>0.278</td><td>0.184</td><td>0.123</td><td>0.083</td><td>0.056</td><td>0.038</td><td>0.026</td><td>0.018</td><td>0.013</td><td>600.0</td><td>9000</td><td>0.004</td><td>0.003</td><td>0.002</td><td>0.001</td><td>. 22</td></th<>	22	0.647	0.422	0.278	0.184	0.123	0.083	0.056	0.038	0.026	0.018	0.013	600.0	9000	0.004	0.003	0.002	0.001	. 22
0.629         0.390         0.247         6.158         0.102         0.066         0.013         0.013         0.006         0.004         0.013         0.006         0.004         0.013         0.006         0.004         0.013         0.007         0.006         0.004         0.001         0.007         0.001         0.001         0.000         0.001 <th< td=""><td>23</td><td>0.634</td><td>0.406</td><td>0.262</td><td>0.170</td><td>0.112</td><td>0.074</td><td>0.049</td><td>0.033</td><td>0.022</td><td>0.015</td><td>0.010</td><td>0.007</td><td>0.002</td><td>0.003</td><td>0.002</td><td>0.002</td><td>0.000</td><td>23</td></th<>	23	0.634	0.406	0.262	0.170	0.112	0.074	0.049	0.033	0.022	0.015	0.010	0.007	0.002	0.003	0.002	0.002	0.000	23
0.610         0.375         0.233         0.146         0.095         0.038         0.014         0.010         0.000 <th< td=""><td>24</td><td>0.622</td><td>0.390</td><td>0.247</td><td>0.158</td><td>0.102</td><td>990.0</td><td>0.043</td><td>0.028</td><td>0.019</td><td>0.013</td><td>0.008</td><td>9000</td><td>0.004</td><td>0.003</td><td>0.002</td><td>0.001</td><td>0.000</td><td>24</td></th<>	24	0.622	0.390	0.247	0.158	0.102	990.0	0.043	0.028	0.019	0.013	0.008	9000	0.004	0.003	0.002	0.001	0.000	24
0.586         0.361         0.220         0.135         0.084         0.053         0.031         0.014         0.009         0.006         0.004         0.005         0.001         0.001         0.001         0.000         0.000         0.000         0.001         0.001         0.001         0.000         0.000         0.001         0.001         0.001         0.000         0.000         0.001         0.000 <th< td=""><td>25</td><td>0.610</td><td>0.375</td><td>0.233</td><td>0.146</td><td>0.092</td><td>0.059</td><td>0.038</td><td>0.024</td><td>0.016</td><td>0.010</td><td>0.007</td><td>0.005</td><td>0.003</td><td>0.002</td><td>0.001</td><td>0.001</td><td>0.000</td><td>25</td></th<>	25	0.610	0.375	0.233	0.146	0.092	0.059	0.038	0.024	0.016	0.010	0.007	0.005	0.003	0.002	0.001	0.001	0.000	25
0.586         0.347         0.207         0.125         0.045         0.047         0.018         0.011         0.007         0.001         0.002         0.001         0.001         0.001         0.000 <th< td=""><td>26</td><td>0.598</td><td>0.361</td><td>0.220</td><td>0.135</td><td>0.084</td><td>0.053</td><td>0.033</td><td>0.021</td><td>0.014</td><td>0.009</td><td>900.0</td><td>0.004</td><td>0.002</td><td>0.002</td><td>0.001</td><td>0.001</td><td>0.000</td><td>- 26</td></th<>	26	0.598	0.361	0.220	0.135	0.084	0.053	0.033	0.021	0.014	0.009	900.0	0.004	0.002	0.002	0.001	0.001	0.000	- 26
0.574         0.333         0.196         0.116         0.0642         0.042         0.016         0.006         0.004         0.006         0.002         0.004         0.002         0.001         0.001         0.000         0.000         0.000           0.563         0.321         0.185         0.107         0.063         0.032         0.014         0.008         0.005         0.001         0.001         0.001         0.000         0.	27.	0.586	0.347	0.207	0.125	9200	0.047	0.029	0.018	0.011	0.007	0.005	0.003	0.002	0.001	0.001	0.001	0.000	. 27
0.563 0.321 0.185 0.107 0.063 0.037 0.022 0.014 0.008 0.005 0.003 0.002 0.001 0.001 0.000	28	0.574	0.333	0.196	0.116	690.0	0.042	0.026	0.016	0.010	9000	0.004	0.002	0.002	0.001	0.001	0.000	0.000	28
0.552 0.308 0.174 0.099 0.057 0.033 0.020 0.012 0.007 0.004 0.003 0.002 0.001 0.001 0.000	29	0.563	0.321	0.185	0.107	0.063	0.037	0.022	0.014	0.008	0.005	0.003	0.002	0.001	0.001	0.000	0.000	0.000	29
0.500 0.253 0.130 0.068 0.036 0.019 0.010 0.006 0.003 0.002 0.001 0.000	30	0.552	0.308	0.174	0.099	0.057	0.033	0.020	0.012	0.007	0.004	0.003	0.002	0.001	0.001	0.000	0.000	0.000	30
0.453 0.208 0.097 0.046 0.022 0.011 0.005 0.003 0.001 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000	32	0.500	0.253	0.130	0.068	0.036	0.019	0.010	900.0	0.003	0.002	0.001	0.001	0.000	0.000	0.000	0.000	0.000	35
	40	0.453	0.208	0.097	0.046	0.022	0.011	0.005	0.003	0.001	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	40